

Turbine :-

→ It is a device which converts hydro power to shaft power.

Classification :-

1. According to type of energy inlet there are two types of turbine.

(a) Impulse Turbine

At inlet of turbine kinetic Energy of water is available.

Ex:- Pelton Wheel Turbine

(b) Reaction Turbine

At inlet of turbine kinetic energy as well as pressure energy of water is available.

Ex:- Francis Turbine, Kaplan Turbine.

2. According to direction of flow there are four types of turbine

(a) Tangential Flow Turbine

(b) Axial flow Turbine

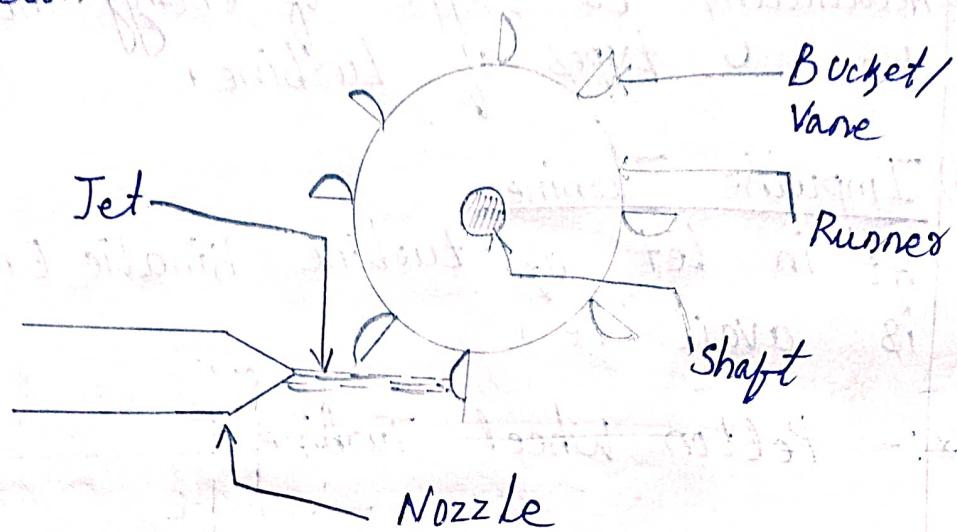
(c) Radial flow Turbine

(d) Mixed (Radial and Axial) Flow Turbine

(a) Tangential Flow Turbine :-

→ Water strikes the runner tangential to the path of rotation of the runner.

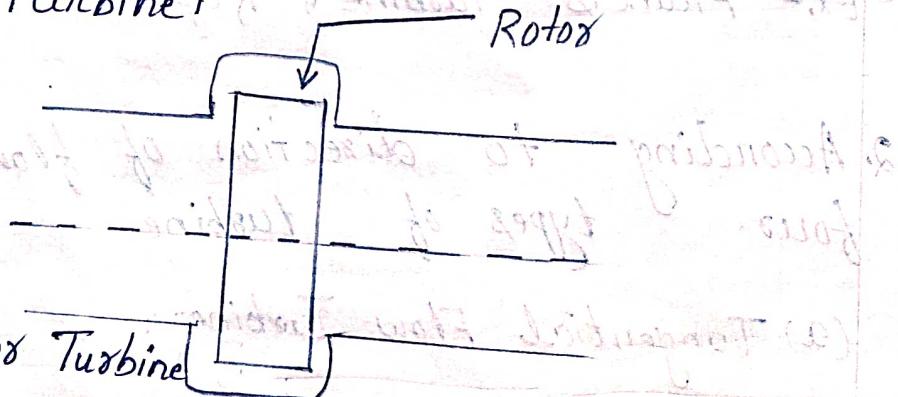
Ex:- Pelton wheel Turbine



(b) Axial Flow Turbine :-

→ Water flow in the direction parallel to axis of the turbines.

Ex:- Propeller Turbine



(c) Radial Flow Turbine :-

→ Water flow in the radial direction through the runner.

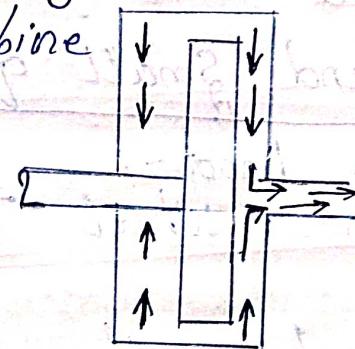
It devide into two types

1. Radially Inward flow turbine
2. Radially outward flow turbine

1. Radially Inward flow Turbine :-

Water coming from outside or outer periphery and it's moving inside.

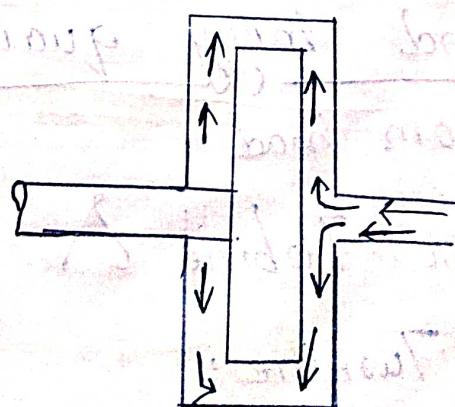
Ex:- Francis Turbine



2. Radially outward flow Turbine :-

Water enter at a center path and water is flowing towards the outward direction.

Ex:- Fourneyron Turbine



(d) Mixed (Radial and axial) Flow Turbine :-

Water flows through the runner in the radial direction but leaves in the direction parallel to axis of rotation!

Ex:- Modern Francis Turbine,

* According to water head and quantity of water it is divided into three types.

(a) High head and small quantity of water flow

Above 250 m head

Ex:- Pelton Wheel Turbine

(b) Medium head and Medium quantity of water flow :-

60 to 250 m head

Ex:- Modern Francis turbine

(c) Low head and large quantity of water flow

Below 60 m head;

Ex:- Propeller Turbine

Kaplan Turbine

* According to the Specific Speed of Turbine :-

(a) Low Specific Speed :-

Specific Speed less than 60.

Ex:- Pelton wheel turbine

(b) Medium Specific Speed :-

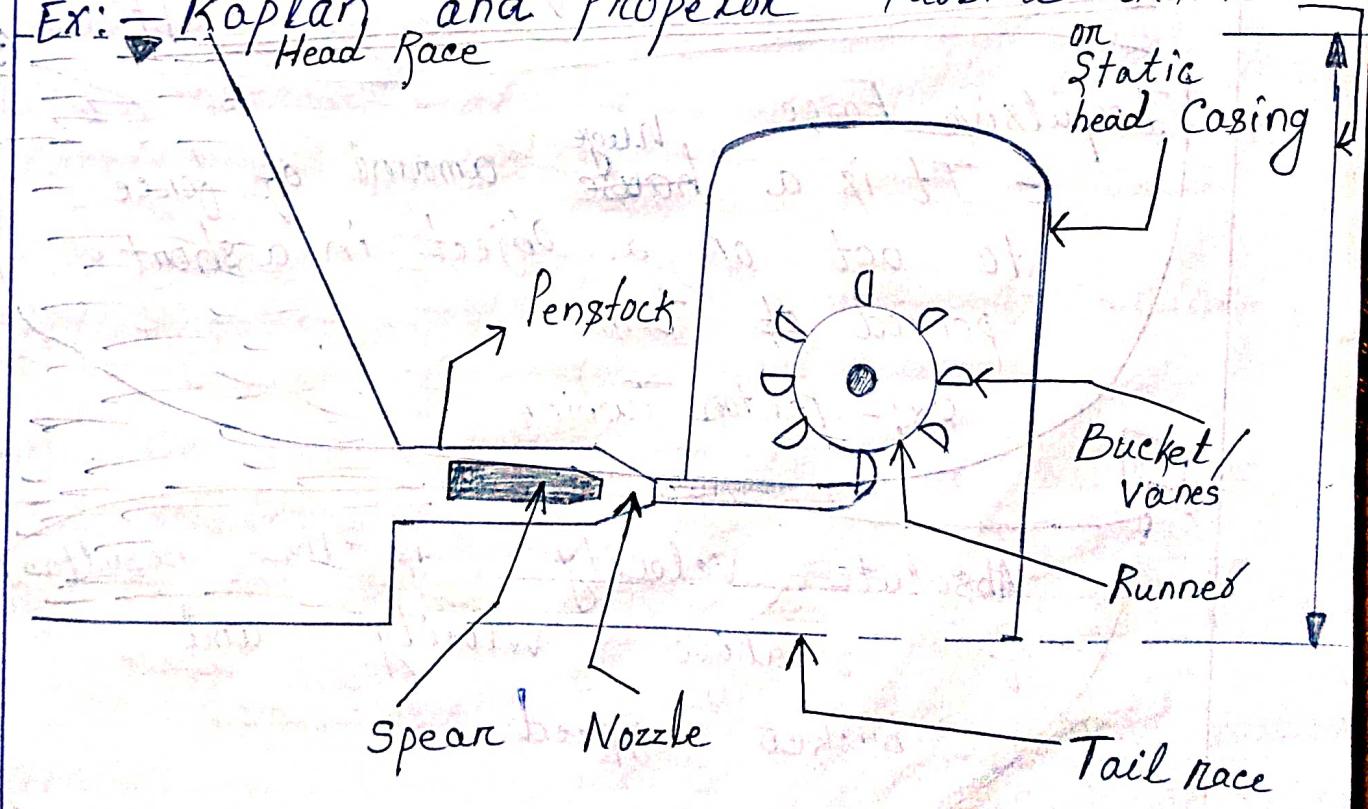
Specific Speed 60 to 400

Ex:- Francis turbine

(c) High Specific Speed :-

Specific Speed More than 400

Ex:- Kaplan and Propellor Turbine, Gross head
Head Race



Working principle and construction of pelton wheel turbine :-

- The pelton wheel turbine is a tangential flow impulse turbine.
- The water strikes the bucket along the tangent of the runner.
- The energy available at the inlet of the turbine is only kinetic energy.
- The pressure available at the inlet of the turbine is zero and outlet of the turbine is atmospheric.
- The turbine is used for high heads.
- The water from the reservoir flows through the penstocks at the outlet of which a nozzle is fitted.
- The nozzle increases the K.E of water following through penstocks.
- At the outlet of nozzle the water comes out in the form of the jet and it's strikes the bucket (cavans) of the runner.
- The main parts of the pelton wheel turbine are

- (i) Nozzle and Flow regulating arrangement (Spear)
 - (ii) Runner and buckets
 - (iii) Casing
 - (iv) Breaking jet
- (i) Nozzle and Flow regulating arrangement (Spear)

- The amount water striking the buckets of the runner is controlled by providing the spear in the nozzle.
- The spear is a conical needle that is operated either by a hand wheel or automatically in an axial direction.
- When the spear is pushed forward into the nozzle the amount of water striking the runner is reduced.
- On the other hand if the spear is pushed back, the amount of water striking the runner increases.

(ii) Runner and Buckets

- It consists of a circular disc on the periphery of which a number of buckets are fixed.
- The shape of the buckets is of a double hemispherical cup or bowl.
- Each bucket is divided into 2 geometrical parts by a dividing wall which is known as spliter.
- Each Bucket is The spliter divides it into two equal parts and the jet comes out at the outer edge of the bucket.
- The buckets are shaped in such a way that the jet gets deflected through 160° or 170° .
- The buckets are made of cast iron, cast steel, bronze or stainless steel depending upon the head at the inlet of the turbine.

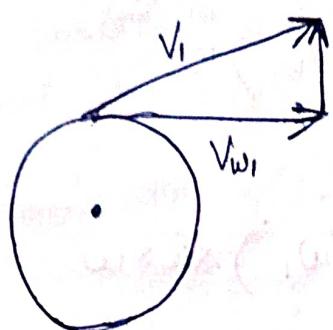
(iii) Casing :-

- The function of the casing is to prevent the splashing of the water and to discharge water to tail race.
- It also acts as a safe guard against accident.
- It is made up cast iron or fabricated steel plates.
- The casing of the pelton wheel does not perform any hydrolic functions.

(iv) Breaking jet :-

- When the nozzle is completely close by the move of spear in the forward direction the amount of water striking the runner reduces to zero. But the runner due to inertia goes on revolving for a long time to stop the runner in a short time a small nozzle is provided which directs the jet of water on the back of the vanes. This jet of water is called breaking jet.

STEADY FLOW:- whose properties doesn't change at any section with respect to time.

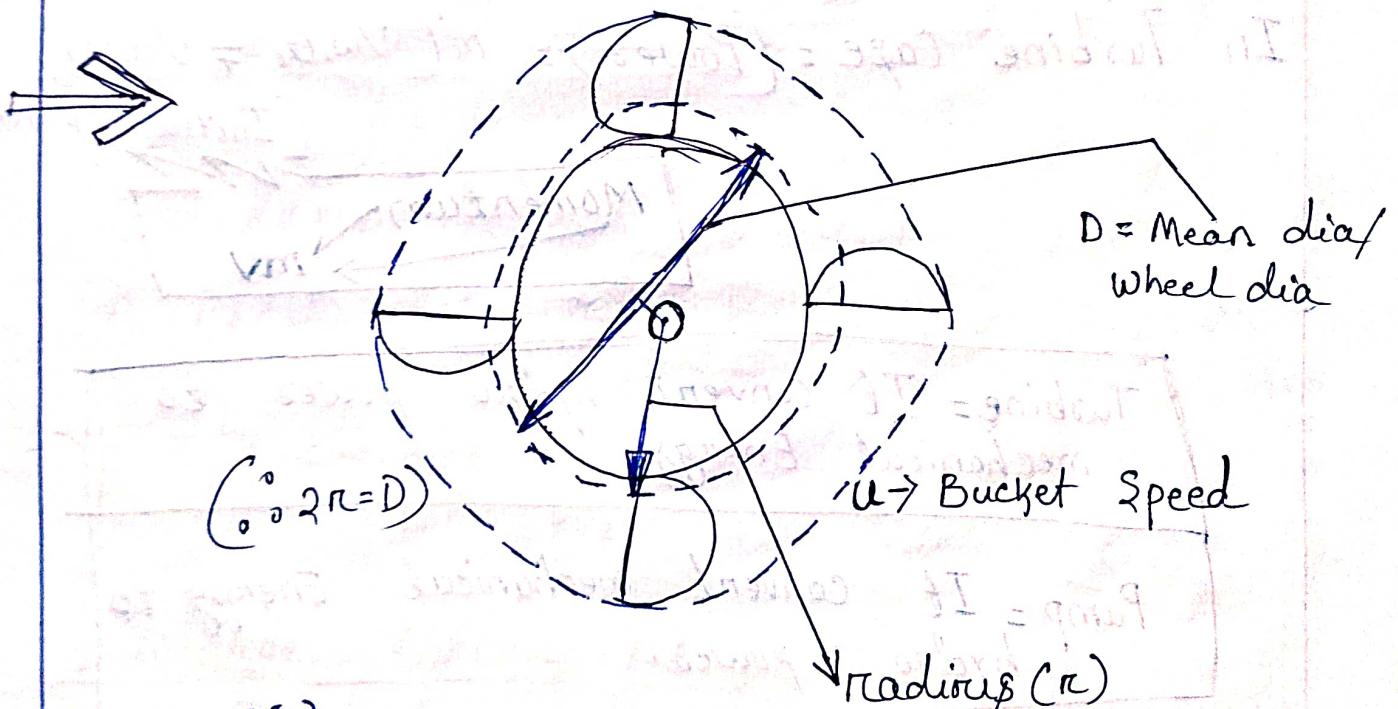


V_i = Actual/Absolute Velocity

V_fi , V_f = Flow Velocity

V_wi = Whirl Velocity

Whirl Velocity = It rotates the rotor



$$u = \omega r$$

$$= \pi \times \frac{2\pi N}{60}$$

$$u = \frac{\pi DN}{60} \text{ m/s}$$

Torque = Rate of change of tangential angular momentum

$$T = F \cdot r$$

$$\Rightarrow F = ma \cdot r$$

$$\Rightarrow T = m \left(\frac{v-u}{t} \right) \cdot r \Rightarrow T = \frac{m}{t} (\text{Final - Initial}) \cdot r$$

$$\Rightarrow T = \dot{m} (Vw_2 - Vw_1) r$$

$$\text{Power} = T \cdot \omega$$

$$= \dot{m} (Vw_2 - Vw_1) \times r \times \omega$$

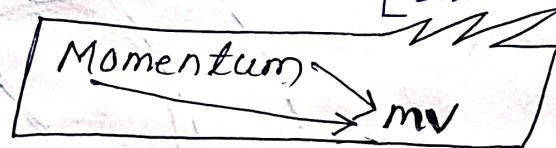
$$[r \times \omega = u]$$

$$= \dot{m} (Vw_2 - Vw_1) \times u \text{ w/s}$$

$$\text{Pump Power} = \dot{m} (Vw_2 u_2 - Vw_1 u_1) \text{ w/s} \quad [\text{Final - Initial}]$$

In Turbine Case = (Power) = $\dot{m} (Vw_1 u_1 - Vw_2 u_2)$

[Initial - Final]



Turbine = It converts hydro power to mechanical Energy.

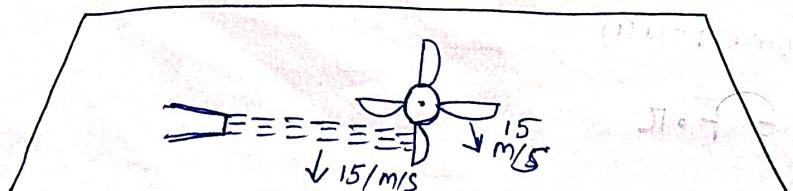
Pump = It converts mechanical Energy to hydro power.

Relative Velocity :-

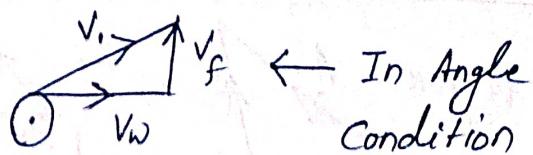
$$t=0.5 \quad v=15 \text{ m/s}$$

$$v=5 \text{ m/s}$$

$$\vec{V}_{AB} = \vec{V}_A - \vec{V}_B = 15 - 5 = 10 \text{ m/s}$$



Velocity-



In Angle Condition

V_f = Flow Velocity

V_w = Wheel Velocity

V_i = Velocity of Jet

Tangential Force Acting on the wheel

$$\text{Power} = m(C V_w, V_i - V_{w_2} u_2)$$

$$\text{Power} = T \times \omega$$

$$\text{Torque}(T) = f_t \times r$$

$$P = f_t \times r \times \omega$$

$$\Rightarrow F_t \times r \times \omega = m(C V_w, V_i - V_{w_2} u_2)$$

$$\Rightarrow F_t \times r = m(C V_w, V_i - V_{w_2} u_2)$$

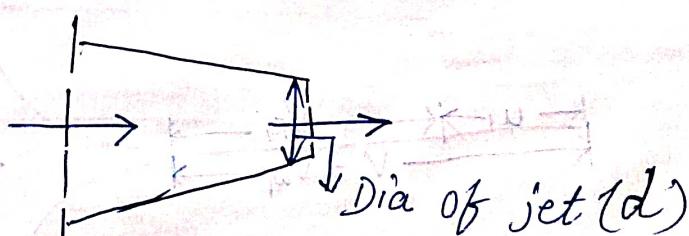
$$\Rightarrow F_t = \frac{m \cdot r (V_w, V_i - V_{w_2})}{\omega}$$

$$\Rightarrow F_t = m(C V_w, V_i - V_{w_2})$$

$$\omega = \frac{\pi N}{60}$$

$$[u = u_1 = u_2]$$

Discharge through Nozzle

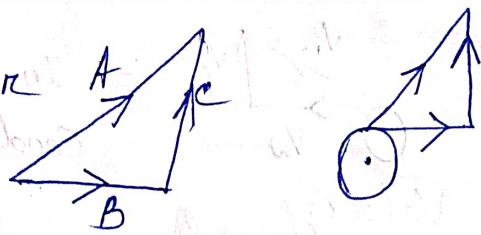


$$\begin{aligned}\text{Discharge}(Q) &= A \times V \\ &= \frac{\pi}{4} d^2 V\end{aligned}$$

$$\text{No of Nozzles} = n$$

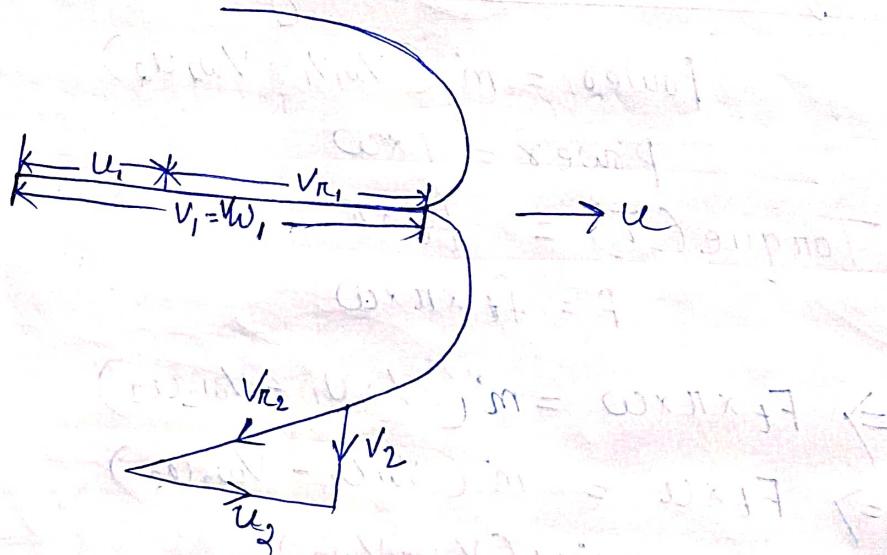
$$Q = n \times \frac{\pi}{4} d^2 \times V_i$$

Triangle
law of Vector
Addition

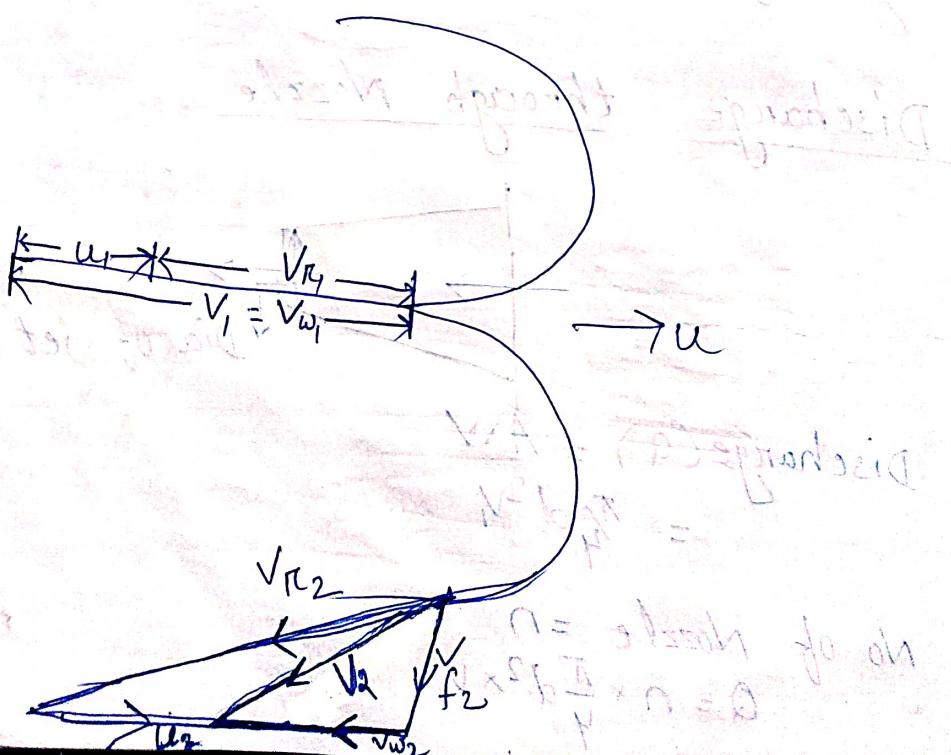


3 Possibility

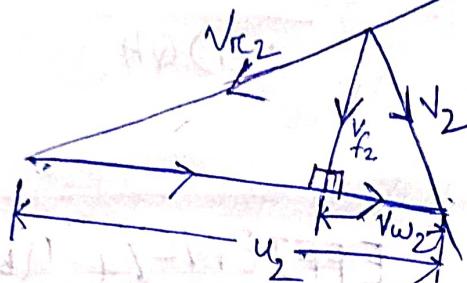
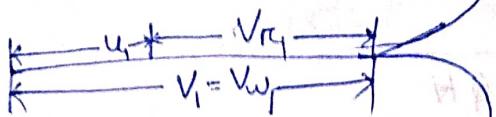
Case I



Case 2



Case - 3

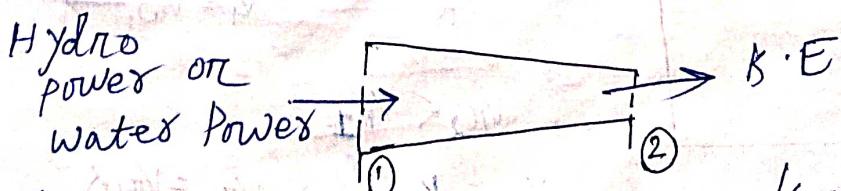


Efficiency (η) :- It is the ratio of the useful work performed by a machine,

$$\eta = \frac{\text{Out Put}}{\text{In Put}}$$

1. Nozzle Efficiency
2. Blading / Diagram Efficiency
3. Hydraulic Efficiency
4. Mechanical Efficiency

I. Nozzle Efficiency (η) :-



$$\text{Hydro Power} = \rho g Q H \quad \text{and} \quad K.E = \frac{1}{2} m v^2$$

$$\eta_N = \frac{\text{out put}}{\text{In Put}} = \frac{\rho_2 m v_1^2}{\beta g Q H} \quad \boxed{\begin{array}{l} \text{Specific weight} \\ \Rightarrow \beta g = \omega \end{array}}$$

$$= \frac{m v_1^2}{2} \times \frac{1}{\beta g Q H} \\ = \frac{m v_1^2}{2 \beta g Q H} = \frac{m v_1^2}{2 \omega Q H}$$

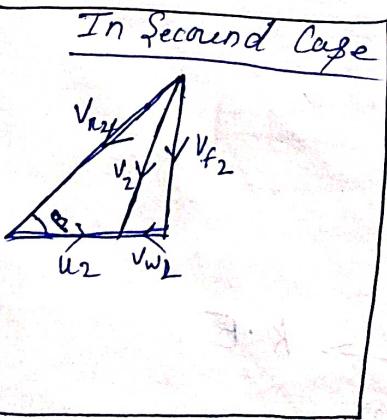
BLADING / DIAGRAM EFFICIENCY (η_b):-

$$\eta_b = \frac{\text{O/P}}{\text{I/P}} = \frac{\text{Power Developed by the runner}}{\text{Kinetic Energy}}$$

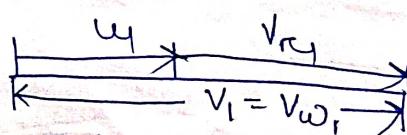
$$= \frac{m (V_{w1} U_1 - V_{w2} U_2)}{\frac{1}{2} m v_1^2}$$

$$= \frac{2 (V_{w1} U_1 - V_{w2} U_2)}{v_1^2}$$

In Max. Efficiency, $\eta_{b\max} = \frac{2 (V_{w1} + V_{w2}) u}{v_1^2}$



Blade Co-efficient of bifurcation (K)



$$\therefore V_{r2} < V_{r1} \\ \frac{V_{r2}}{V_{r1}} = K \Rightarrow V_{r2} = V_{r1} K$$

When Smooth Surface (K) I

$$V_1 = U_1 + V_{R1}$$

$$\Rightarrow V_{R1} = V_1 - U_1$$

$$V_{R2} = K(V_1 - U_1)$$

In this right Angle triangle,

$$\cos \beta = \frac{b}{h} = \frac{U_2 + V_{W2}}{V_{R2}}$$

$$\Rightarrow V_{R2} \cos \beta = U_2 + V_{W2}$$

$$\Rightarrow V_{W2} = V_{R2} \cos \beta - U_2$$

\therefore Put it in Power or
Maximum Power in the Nozzle Blade

$$P = \frac{2(V_1 + V_{R2} \cos \beta - U) U}{V_1^2}$$

$$= \frac{2U}{V_1^2} (V_1 + V_{R2} \cos \beta - U)$$

$$= \frac{2U}{V_1^2} [(V_1 - U) + K(V_1 - U) \cos \beta]$$

$$= \frac{2U}{V_1^2} (V_1 - U) \{ 1 + K \cos \beta \}$$

$$= \frac{2UV_1}{V_1^2} - \frac{2U^2}{V_1^2} (1 + K \cos \beta)$$

$$= \frac{2U}{V_1} - \frac{2U^2}{V_1^2} (1 + K \cos \beta)$$

$$= 2\beta - 2\beta^2 (1 + K \cos \beta)$$

$$\therefore = 2(\beta - \beta^2)(1 + K \cos \beta)$$

\therefore Derivative max or minimum

\therefore Blade Speed
ratio = (β)
 $= \frac{U}{V_1}$

It is the ratio of blade
speed or nozzle
velocity

$$\frac{d\eta_b}{d\beta} = 0$$

$$\Rightarrow 2(1+k \cos \beta_2) \frac{d(1-\beta^2)}{d\beta} = 0$$

$$\Rightarrow 2(1+k \cos \beta_2)(1-2\beta^2) = 0$$

$$\Rightarrow 1-2\beta^2 = 0 \Rightarrow 2\beta = 1 \Rightarrow \beta = \frac{1}{2}$$

\therefore put the value of β in equation 1

$$2\left(\frac{1}{2} - \frac{1}{4}\right)(1+k \cos \beta_2)$$

$$= 2\left(\frac{1}{4}\right)(1+k \cos \beta_2)$$

$$= \frac{3}{4}(1+k \cos \beta_2)$$

$$= \frac{1+k \cos \beta_2}{2}$$

$K = \text{Smooth Surface}$

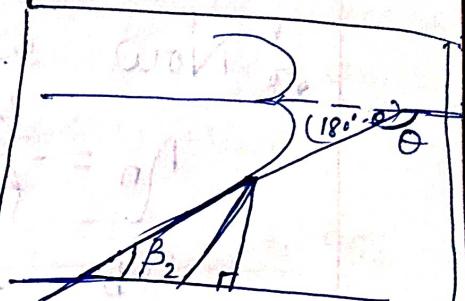
$$\therefore \eta_b = \frac{1+k \cos \beta_2}{2}$$

$$\therefore \text{If } K=1, \text{ then } \eta_b = \frac{1+k \cos \beta_2}{2} = \frac{1+\cos \beta_2}{2}$$

Hydraulic Efficiency (η_h)

$$\eta_h = \frac{O.P}{I.P} = \frac{\text{Runner Power}}{\text{Water Power}}$$

$$= \frac{m(V_w u_1 + V_w u_2)}{\rho g Q H}$$



If we consider,

$$\eta_n \times \eta_b = \frac{K.E}{W.P} \times \frac{P_{\text{runner}}}{K.E}$$

$$= \frac{P_{\text{runner}}}{W.P} = \eta_h$$

θ = Angle of deflection

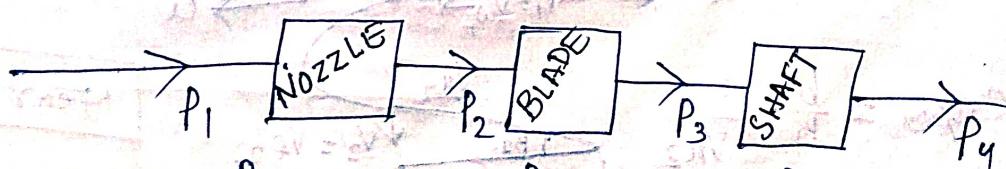
Generally $\beta_2 = 15^\circ$
we consider

If we neglecting η_n or $\eta_n = 1$ → Frictionless
then, $\eta_b = \eta_h$

Mechanical Efficiency (η_m)

$$\eta_m = \frac{O.P}{I.P} = \frac{\text{Shaft Power}}{\text{Runner Power}}$$

Calculating overall Efficiency of a Body:-



$$\eta_N = \frac{P_2}{P_1}, \quad \eta_B = \frac{P_3}{P_2}, \quad \eta_S = \frac{P_4}{P_3}$$

$$\therefore \eta_{N.B} = \frac{P_2}{P_1} \times \frac{P_3}{P_2} = \frac{P_3}{P_1}$$

∴ Overall Efficiency ($\eta_{N.B.S}$ or η_0) = $\eta_p \times \eta_b \times \eta_m$

$$\eta_p = \frac{P_2}{P_1} \times \frac{P_3}{P_2} \times \frac{P_4}{P_3} = \frac{P_4}{P_1}$$

∴ Now we put Pelton wheel turbine,

$$\eta_b = \frac{\frac{1}{2}mv^2}{\rho g Q H}$$

$$\eta_b = \frac{\text{Runner Power}}{\frac{1}{2}mv^2} = \frac{m u (V_{w1} - V_{w2})}{\frac{1}{2}mv^2}$$

$$\eta_m = \frac{\text{Shaft Power}}{\text{Runner Power}} = \frac{\text{Shaft Power}}{m(V_{w1} - V_{w2})u}$$

∴ Overall Efficiency (η_0) =

$$\frac{K.E}{W.P} \times \frac{\text{Runner Power}}{K.E} \times \frac{\text{Shaft Power}}{\text{Runner Power}}$$

$$\eta_0 = \frac{\text{Shaft Power}}{\text{Water Power}}$$

If I consider β_2 in 3 possibility for angle

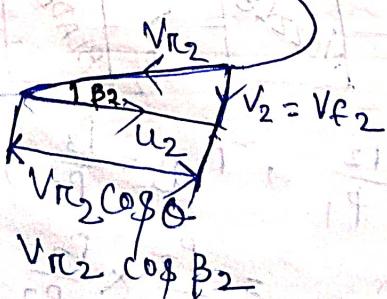
In case 1-



$$\therefore \cos \theta = \frac{b}{h} = \frac{u_2}{V_{r2}}$$

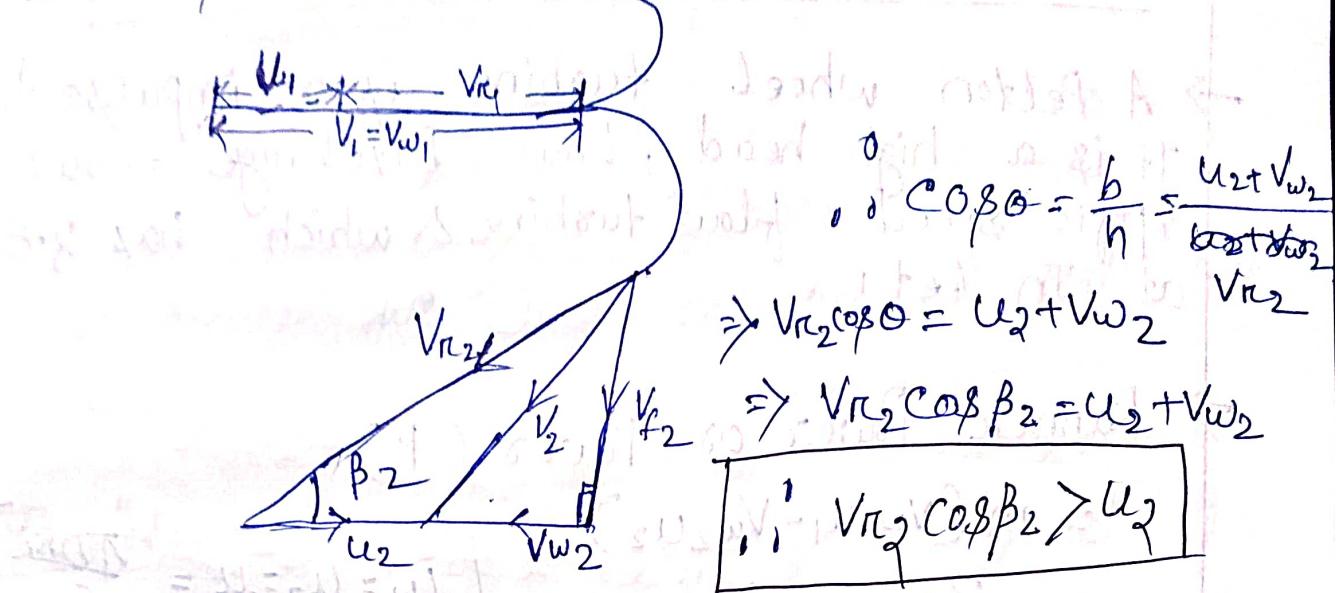
$$\Rightarrow V_{r2} \cos \theta = u_2$$

$$\Rightarrow V_{r2} \cos \beta_2 = u_2$$

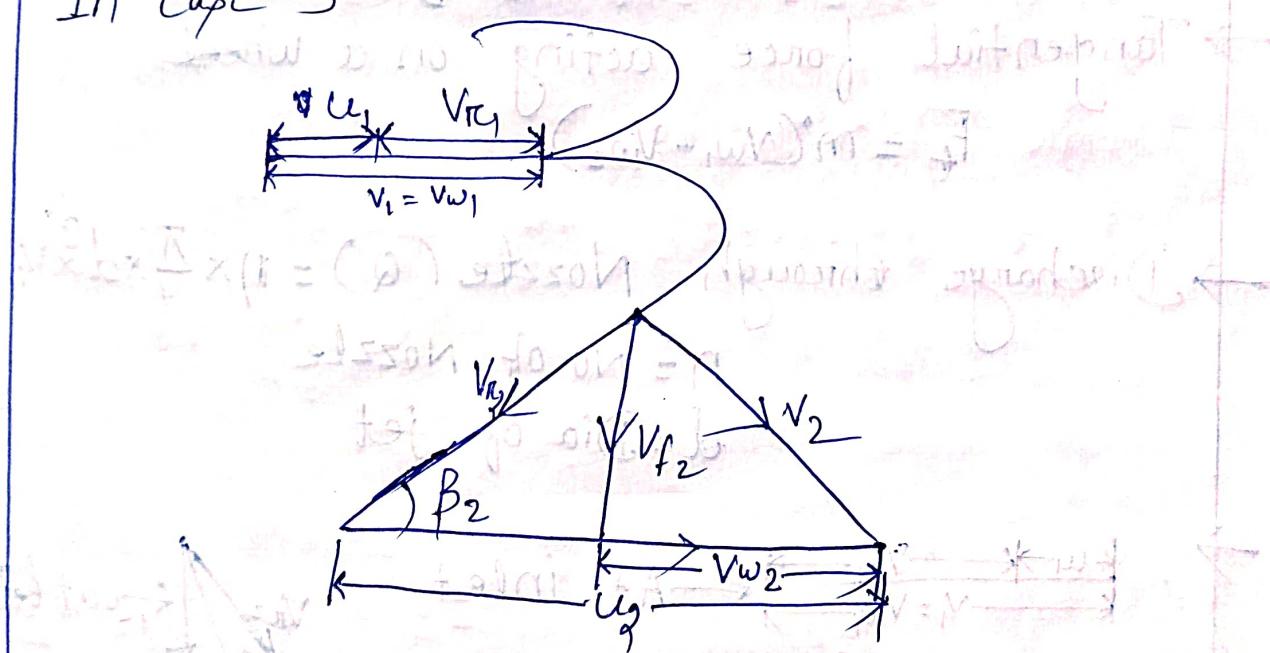


$$\text{Hence } u_2 = u$$

In Case - 2 Inlet angle is less than



In case - 3



$$\therefore \cos \beta_2 = \frac{b}{h} = \frac{u_2 - v_{w2}}{V_{r2}}$$

$$\Rightarrow V_{r2} \cos \beta_2 = u_2 - v_{w2}$$

$\Rightarrow u_2 > V_{r2} \cos \beta_2$

Overview in Pelton Wheel turbine :-

→ A Pelton wheel turbine is a impulse turbine. It is a high head, Low Discharge, Low specific speed flow turbine which has K.E at Inlet.

→ Running Power or Power (P)

$$= m(V_{w1}u_1 - V_{w2}u_2) \quad [u_1 = u_2 = u = \frac{\pi D N}{60}]$$

$$= m(V_{w1} - V_{w2})u$$

D = wheel Dia

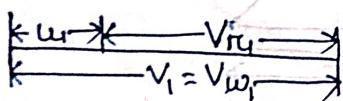
→ Tangential force acting on a wheel

$$F_t = m(V_{w1} - V_{w2})$$

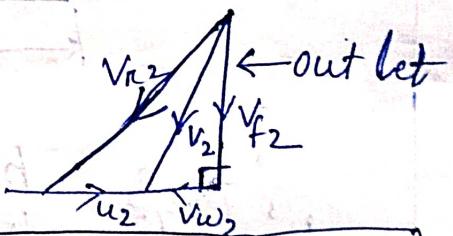
→ Discharge through Nozzle (Q) = $n \times \frac{\pi}{4} \times d^2 \times V_f$

n = NO of Nozzle

d = Dia of jet



At inlet



$$V_{R1} > V_{R2} \Rightarrow \frac{V_{R2}}{V_{R1}} < 1$$

$$\frac{V_{R2}}{V_{R1}} = k$$

$$\therefore V_{R2} = k V_{R1}$$

k = Blade Co-efficient of friction

When "k" is smooth surface then

$$[k = 1]$$

→ Blade Speed ratio (s) = $\frac{u}{V_1}$

V_1 = Velocity at inlet

u = water jet



Why we calculate Efficiency?

→ Because we know the machine performance.

In Pelton Wheel turbine Some Problems :-

Problem No-1

The bucket speed of pelton wheel turbine 15 m/s the rate of flow of water under a Head of 42 m is $1 \text{ m}^3/\text{s}$. If the jet is deflected by 165° Find the power and hydraulic efficiency of turbine.

Take,

$$C_V = 0.985$$

Given Data:-

$$\text{Bucket Speed } (u) = 15 \text{ m/s}$$

$$\text{Head } (H) = 42 \text{ m}$$

$$\text{Power } (P) = ??$$

$$\text{Discharge } (Q) = 1 \text{ m}^3/\text{s}$$

$$\eta_h = ??$$

$$\text{Angle } (\beta_2) = 180^\circ - 160^\circ = 15^\circ$$

$$\therefore \beta_2 = 15^\circ$$

$$C_V = 0.985$$

$$V_1 = C_V \sqrt{2gh} = (0.985) \sqrt{2 \times 9.81 \times 42} \text{ m/s}$$

$$= 28.27 \text{ m/s}$$

, we know that $V_1 = V_{w1}$

mass flow rate (m') = $\rho_{av} A$ [$av = Q$]

$$= \rho Q$$

[Hence Water Density = 1000]

~~$= 0.53 \times$~~

$$= 1000 \times 1 = 1000 \text{ kg/s}$$

$$\therefore V_{r2} = V_1 - w_1 = 28.27 - 15 = 13.27 \text{ m/s}$$

$V_{r2} = V_{r1}$ [Inlet velocity = outlet Velocity]

$$\therefore V_{r2} \cos \beta_2 = 13.27 \times \cos(15^\circ) = 12.81 \text{ m/s}$$

Hence $u > V_{r2} \cos \beta_2$

$$\therefore u - V_{w2} = V_{r2} \cos \beta_2$$

$$\Rightarrow V_{w2} = u - V_{r2} \cos \beta_2$$

$$= 15 - 12.81 = 2.19 \text{ m/s}$$

$$\therefore \text{Power} = m'(V_{w1} - V_{w2})u$$

$$= 1000 (28.27 - 2.19) 15 \quad [V_1 = V_{w1}]$$

$$= 391200 \text{ W}$$

$$= \frac{391200}{1000} = 391.2 \text{ kW}$$

Hydrolic Efficiency (η_h)

$$\therefore \eta_h = \frac{\text{R.Power}}{\text{Water Power}} = \frac{391200}{1000 \times 9.81 \times 1 \times 42} = 0.94 = 94\%$$

The Power is 391.2 kW and the hydrolic efficiency is (η_h) 94%.

Problem No-02

A Pelton wheel turbine is to be designed for the following specification:-

$$\text{Shaft Power (S.P)} = 11772 \text{ kW}$$

$$\text{Head (H)} = 380 \text{ m}$$

$$\text{Speed (N)} = 750 \text{ r.p.m}$$

and overall efficiency ~~is~~ 86% and jet diameter is not to exceed $\frac{1}{6}$ of the wheel diameter. Determine wheel diameter, Dia of the jet and number of nozzle required.

Given Data:-

$$S.P = 11772 \text{ kW}$$

$$H = 380 \text{ m}$$

$$N = 750 \text{ r.p.m}$$

$$\eta_0 = 86\%$$

$$d = \frac{1}{6} D, C_V = 0.985$$

$$D = ??$$

$$d = ??$$

$$n = ??$$

$$V_i = C_V \sqrt{2gH} = 0.985 \sqrt{2 \times 9.81 \times 380} = 85.05 \text{ m/s}$$

$$f = \frac{u}{V_i}$$

$$\Rightarrow 0.45 = \frac{u}{85.05} \Rightarrow u = 85.05 \times 0.45 = 38.27$$

$$\text{we know, } u = \frac{\pi D N}{6}$$

$$\Rightarrow 38.27 = \frac{\pi \times D \times 750}{60}$$

$$\Rightarrow \frac{38.27 \times 60}{\pi \times 750} = D \Rightarrow D = 0.97 \text{ m}$$

In question, $d = \frac{1}{6} D$
 $= \frac{1}{6} \times 0.97 = 0.164 \text{ m}$

∴ We know that

$$\eta_0 = \frac{\text{Shaft Power}}{\text{Water Power}}$$

$$\Rightarrow \frac{86}{100} = \frac{11772 \text{ k.W}}{1000 \times 9.81 \times 380 \times Q} \Rightarrow \frac{86}{100} = \frac{11772 \times 1000}{1000 \times 9.81 \times 380 \times Q}$$
$$\Rightarrow 86 \times 9.81 \times 36 \times Q = 11772 \times 100$$
$$\Rightarrow Q = \frac{11772 \times 100}{86 \times 9.81 \times 36} = 3.67 \text{ m}^3/\text{s}$$

∴ Discharge (Q) = $n \times \frac{\pi}{4} d^2 v$

$$\Rightarrow 3.67 = n \times \frac{\pi}{4} \times (0.164)^2 \times 85.05$$

$$\Rightarrow 3.67 = n \times \frac{\pi}{4} \times 0.0256 \times 85.05$$

$$\Rightarrow n = \frac{3.67}{1.710031713}$$

$$\Rightarrow n = 2.14 = 2$$

∴ wheel Dia (D) = 0.97

Jet Dia (d) = 0.164

And Number of Number Required = 2

All unit of the water Discharge

$$\frac{\text{kg}}{\text{m}^3} \times \frac{\text{m}}{\text{s}^2} \times \frac{\text{m}^3}{\text{s}} \times \text{m}$$

$$f \times g \times Q \times H$$

$$\frac{\text{kg} \cdot \text{m}^2}{\text{s}^3} = \frac{\text{kg} \cdot \text{m}}{\text{s}^2} \times \frac{\text{m}}{\text{s}} = \underline{N \times \frac{\text{m}}{\text{s}}} \rightarrow \frac{\text{J}}{\text{s}}$$

$$\therefore J = \frac{\text{kg} \cdot \text{m}^2}{\text{s}^2}$$

$$N = \frac{\text{kg} \cdot \text{m}}{\text{s}^2}$$

$$\frac{\text{Joule}}{\text{sec}} = \text{Watt}$$

$$1 \text{ Watt} = \frac{\text{Joule}}{\text{sec}}$$

Problem No- 03

Two jets strike the buckets of pelton wheel which is having a shaft Power of 15450 kW / The diameter of each jet is 200mm if the Head on turbine is 400m , Find the overall Efficiency . Take $C_v = 1$

Solution:- Given Data:-

$$n = 2$$

$$S.P = 15450 \text{ kW}$$

$$d = 200 \text{ mm} = \frac{200}{1000} = 0.2 \text{ m}$$

$$H = 400 \text{ m}$$

$$C_v = 1$$

$$\therefore V_1 = C_v \sqrt{2gh} = \sqrt{2 \times 9.81 \times 400} = 88.58 \text{ m/s}$$

$$Q = n \times \frac{\pi}{4} \times d^2 \times V$$

$$= 2 \times \frac{\pi}{4} \times 0.2 \times 88.58$$

$$= 5.565 \text{ m}^3/\text{s}$$

∴ Overall Efficiency (η_o) = $\frac{S.P.}{W.P.}$

$$= \frac{S.P.}{S.G.Q.H} = \frac{15450 \times 1000}{1000 \times 9.81 \times 5.565 \times 400} = 0.70 = 70.75\%$$

Problem No-04

A Pelton wheel turbine is receiving water from a penstock with a gross head of 510m. $\frac{1}{3}$ of gross head is lost in friction in the penstock. The rate of flow through the nozzle fitted at the end of penstock is $2.2 \text{ m}^3/\text{s}$. The angle of deflection of jet is 165° . Determine And $S = 0.45 \text{ kg/m}^3$

(i) The Power Given by the water of the runner.

(ii) Hydraulic Efficiency (η_h).

Solution:-

Given Data:-

$$H_g = 510 \text{ m}$$

$$Q = 2.2 \text{ m}^3/\text{s}$$

$$\phi = 180^\circ - 165^\circ = 15^\circ$$

$$\beta_2 = 15^\circ$$

$$\therefore \text{Net head}(H) = \text{Gross Head}(H_g) - (H_f) \text{ Friction Head}$$

$$H = 510 - \frac{510}{3}$$

$$= 510 - 170$$

$$= 340 \text{ m} (\text{downward})$$

$$\rho = 0.45 \text{ kg/m}^3$$

$$V_1 = C\sqrt{2gH}$$

$$= 1 \sqrt{2 \times 9.81 \times 340} = 81.67 \text{ m/s}$$

$$\therefore Q = n \times \frac{\pi}{4} \times d^2 V_1$$

$$= 2.2 \text{ m}^3/\text{s}$$

$$m' = g_x(a \times v) = g_x Q = 0.45 \times 2.2 = 0.9922 \text{ kg/s}$$

\therefore we know bucket speed ratio (β)

$$= \frac{u}{v_1}$$

$$\Rightarrow 0.45 = \frac{u}{81.67}$$

$$\Rightarrow 0.45 \times 81.67 = u$$

$$\Rightarrow u = 36.75 \text{ m/s}$$

In triangle

$$u + v_{r1} = v_1$$

$$\Rightarrow 81.67 = 36.75 + v_{r1}$$

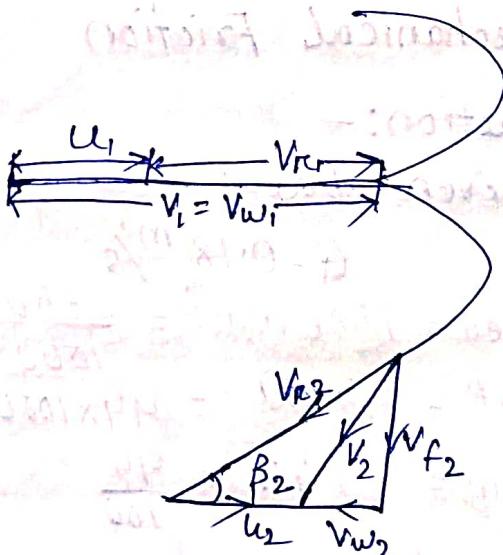
$$\Rightarrow v_{r1} = 81.67 - 36.75$$

$$= 44.9 \text{ m/s}$$

$$\therefore v_{r1} = v_{r2}$$

$$\therefore v_{r2} \cos \beta_2 = 44.9 \times \cos(15^\circ) = 43.37$$

$$\therefore v_{r2} \cos \beta_2 > u$$



$$\begin{aligned}
 \text{Power (P)} &= m(Cv w_1 - Cv w_2) \\
 &= m(Cv w_1 + Cv w_2) U_{OPC} \\
 &= 2200(36.73)88.27 \\
 &= 7132745.62
 \end{aligned}$$

Problem No-05

The following data were obtained from a based on pelton wheel head at the base of nozzle = 32 m, Discharge of nozzle = $0.18 \text{ m}^3/\text{s}$ and area of jet 7500 mm^2 , shaft power 44 kW , Mechanical efficiency 94% . Calculate the power lost -

- (i) In the Nozzle
- (ii) Runner Power
- (iii) Mechanical Friction

Solution:-

Given Data:-

$$Q = 0.18 \text{ m}^3/\text{s}$$

$$\text{Area} = 7500 \text{ mm}^2 = \frac{7500}{1000} = 7.5 \text{ m}^2 = 7.5 \times 10^{-3} \text{ m}^2$$

$$S.P = 44 \text{ kW} = 44 \times 1000 \text{ W}$$

$$\eta_m = 94\% = \frac{94}{100}$$

$$H = 32 \text{ m}$$

$(V_1 = Cv \sqrt{2gH})$ This formula is not applicable in this process.

So,

$$\begin{aligned}
 \text{We know } Q &= A V \\
 \Rightarrow 0.18 &= 7.5 \times 10^{-3} \times V
 \end{aligned}$$

$$\Rightarrow V = \frac{0.18}{7.5 \times 10^{-3}} = 24 \text{ m/s}$$

$$\therefore Q = 0.18,$$

(i) Power inlet of the Nozzle

$$W.P = \dot{m} g Q H$$

$$= 1000 \times 9.81 \times 0.18 \times 32$$

$$= 56505.6 \text{ W}$$

$$= 56505.6 \div 1000 = 56.50 \text{ kW}$$

(ii) Power outlet of the Nozzle

$$K.E = \frac{1}{2} m v^2$$

$$= \frac{1}{2} \times 180 \times (24)^2$$

$$= 51840 \text{ W} = 51.84 \text{ kW}$$

$$\therefore m = \dot{m} = f Q$$

$$= 1000 \times 0.18$$

$$= 180 \text{ kg/s}$$

(iii) Power lost in the Nozzle

$$= W.P - K.E$$

$$= 56.50 - 51.84 = 4.66 \text{ kW}$$

(ii) Runner at inlet is $K \cdot E = 51.84 \text{ k.w}$
at outlet

We know that, $\eta_m = \frac{S \cdot P}{P_R}$

$$\Rightarrow \frac{94}{100} = \frac{44 \times 1000}{P_R}$$
$$\Rightarrow P_R = \frac{44 \times 1000 \times 100}{94} = 46808.510 \text{ h}$$
$$= 46.805 \text{ k.w}$$

\therefore Power lost in Runner
 $= K \cdot W - P_R = 51.84 - 46.805 = 5.035 \text{ k.w}$

(iii) Power lost in mechanical friction

$$(P_R - P_{shf})$$

$$= 46.805 - 44 = 2.805 \text{ k.w}$$

\therefore Power lost in Mechanical friction = 2.805 k.w

\therefore Power lost in Runner = 5.035 k.w

\therefore Power lost in Nozzle = 4.66 k.w

(Ans)

Problem No-06 :- A Single jet in pelton wheel turbine is required to develop a S.P of 10MW the head at the nozzle is 760m and Mechanical efficiency = 0.95, $\eta_h = 87$, $\beta_2 = 15^\circ$, $C_v = 0.97$, $V_{R2} = 0.85 V_{R1}$, calculate

- (i) Discharge (ii) Jet dia (iii) Force exerted on the jet
- (iv) Best Shrinkage Speed for the generator at 50Hz corresponding mean dia of wheel to jet dia $D/d = 10$

Solution:-

Given Data:-

$$S.P = 10 \text{ MW} = 10 \times 10^6 \text{ W}$$

$$H = 760 \text{ m}$$

$$V_{R2} = 0.85 V_{R1}$$

$$\eta_m = 0.95$$

$$n = 100 \text{ Hz}$$

$$\eta_h = 87$$

$$\beta_2 = 15^\circ$$

$$V_1 = C_v \sqrt{2gH} = 0.97 \sqrt{2 \times 9.81 \times 760} = 118.4 \text{ m/s}$$

$$\therefore U = 0.46 \times 118.4 = 54.46 \text{ m/s}$$

$$V_{R1} = V_1 - U = 118.4 - 54.46 = 63.94 \text{ m/s}$$

$$V_{R2} = 0.85 V_1 \Rightarrow V_{R2} = 0.85 \times 63.94 = 54.349 \text{ m/s}$$

$$\therefore V_{R2} \cos \beta_2$$

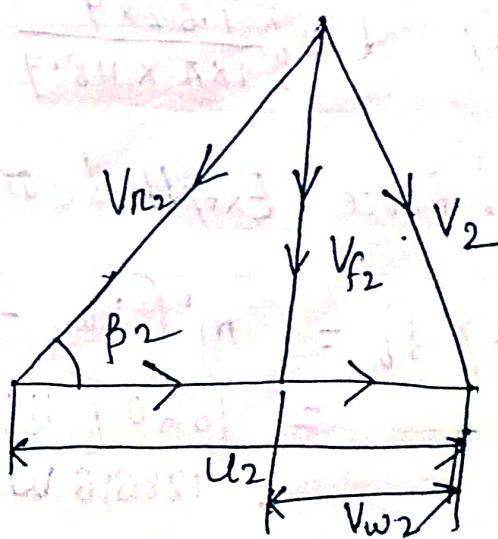
$$\Rightarrow 54.349 \cos 15^\circ = 52.49$$

$$\therefore U > V_{R2} \cos \beta_2$$

$$\therefore \cos \theta = \frac{U_2 - V_{w2}}{V_{R2}}$$

$$\Rightarrow V_{R2} \cos \theta = U_2 - V_{w2}$$

$$\Rightarrow U_2 = V_{R2} \cos \beta_2 + V_{w2}$$



$$\Rightarrow Vw_2 = U_2 - V_{R2} \cos \beta_2$$

$$= 54.46 - 52.49 = 1.97$$

i) We know that

$$\eta_h = \frac{\text{Runner Power}}{\text{Water Power}}$$

$$\& \eta_m = \frac{\text{Shaft Power}}{\text{Runner Power}}$$

$$\therefore \eta_h \times \eta_m = \frac{S.P}{W.P}$$

$$\therefore \frac{0.95 \times 0.87}{100 \times 100} = \frac{10 \times 10^6}{1000 \times 9.81 \times Q \times 760}$$

$$\Rightarrow Q \times 0.95 \times 0.85 \times 1000 \times 9.81 \times 760 = 100 \times 100 \times 10 \times 10^6$$

$$\Rightarrow Q = \frac{100 \times 100 \times 10 \times 10^6}{0.95 \times 0.87 \times 1000 \times 9.81 \times 760} = 1.0629 \text{ m}^3/\text{s}$$

$$\therefore Q = n \times \frac{\pi}{4} d^2 V, \Rightarrow Q = 1 \times \frac{\pi}{4} \times d^2 \times 118.4$$

$$\Rightarrow 1.062 = \frac{1 \times \pi \times 118.4 \times d^2}{4}$$

$$\Rightarrow \frac{1.062 \times 4}{1 \times \pi \times 118.4} = d^2 \quad \therefore m = \rho Q$$

$$\Rightarrow d = \sqrt{\frac{1.062 \times 4}{1 \times \pi \times 118.4}} = 0.13 \text{ m} \quad = 1000 \times 1.062 \text{ kg/s}$$

ii) Force Exerted on the jet (ft)

$$\Rightarrow f_f = m(Vw_1 - Vw_2)$$

$$= 1620 [118.4 - 1.97]$$

$$= 188616 \text{ lb} = 188616 \text{ kg}$$

REACTION TURBINE

$$\therefore \frac{D}{d} = 10 \Rightarrow \frac{D}{0.13} = 10 \Rightarrow D = 10 \times 0.13 = 1.3 \text{ m}$$

$$U = \frac{\pi D N}{60}$$

$$\Rightarrow 54.46 = \frac{\pi \times 1.3 \times N}{60}$$

$$\Rightarrow 54.46 \times 60 = \pi \times 1.3 \times N$$

$$\Rightarrow N = \frac{54.46 \times 60}{\pi \times 1.3} = 802.72 \text{ r.p.m}$$

Form Electrical Engineers.

$$N = \frac{120 F}{P}$$

\therefore Frequency (F) = 50 Hz

$$\Rightarrow 802.72 = \frac{120 \times 50}{P}$$

$$\Rightarrow P = \frac{120 \times 50}{802.72} = 7.47$$

$$\therefore \text{Maximum Speed (N)} = \frac{120 \times 50}{7.47} = 803 \text{ r.p.m}$$

(Ans)

REACTION TURBINE

→ Reaction Turbines are Francis & Kaplan Turbine.

Francis Turbine

→ Construction of Francis Turbine :-

Definition:-

- (1) Francis turbine is a radially inward and Axially outlet flow turbine.
- (2) This turbine operates under medium heads (60-250)m and Medium specific speed (60-400).
- (3) In inlet only kinetic energy and pressure energy present in the turbine.
- (4) It is a medium discharge.

The main parts of the Francis Turbine :-

1. Penstock :- The penstock is also known as the input pipe. The diameter lies between 1 to 10 meters.
 2. Spiral Casing :- It is the inlet to the turbine. The water flowing from the reservoir or dam is made to pass through this pipe with high pressure.
- Which the area of cross-section of the casing is gradually decreasing, The casing completely surrounded runner of the turbine.

3. Guide Vane :- The main function of the guide vane are to guide the water to ward the runner.

→ It converts pressure energy of the fluid into kinetic Energy.

Runner Blades :-

→ In runner the energy from the water it converts to rotational motion of the main shaft.

→ The runner blades design how effectively a turbine is going to perform.

→ The runner blades are divided into two parts :- The lower half is made in the shape of a small bucket so that it uses the impulse action of water to rotate the turbine.

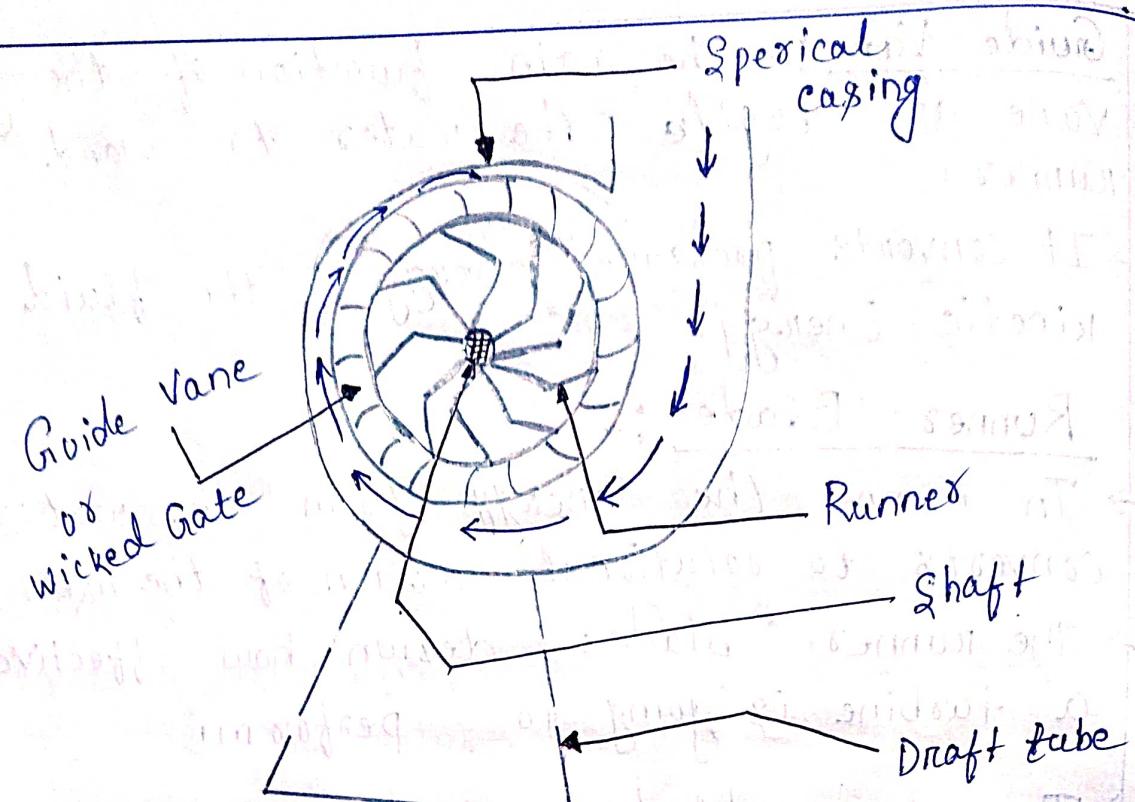
→ The upper parts of the blades uses the reaction force of water flowing through it.

Draft Tube :-

→ The draft tube is an expanding tube is used to discharge the water through the runner and next to the tail race.

→ The main function of the draft tube is to reduce the water velocity at the time of discharge.

→ It's cross-sectional area increases along it's length as the water coming out of the runner blades.

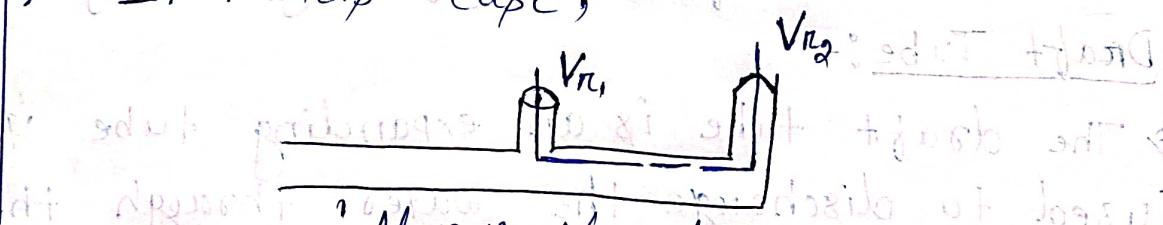


→ In Francis Turbine $C_4 \neq U_2$

$$\therefore C_4 = \frac{\pi D_1 N}{60} \text{ and } C_2 = \frac{\pi D_2 N}{60}$$

→ Runner Power (P_R) = $m \cdot (V_{w1} C_4 + V_{w2} C_2)$

→ In Francis case,



$$\therefore V_{R2} > V_{R1}$$

→ Francis turbine blades or Bucket is 16-20

→ Absolute velocity is the resultant of bucket speed and relative

→ Kaplan turbine Blade or vane is always less than Francis turbine

Efficiency :- $\frac{O/P}{I/P}$

$$\eta_h = \frac{R \cdot P}{W \cdot P} = \frac{P_R}{P_W} = \frac{m (V_{w1} u_1 + V_{w2} u_2)}{\beta g Q H}$$

$V_{w2} = \text{Because axial out}$

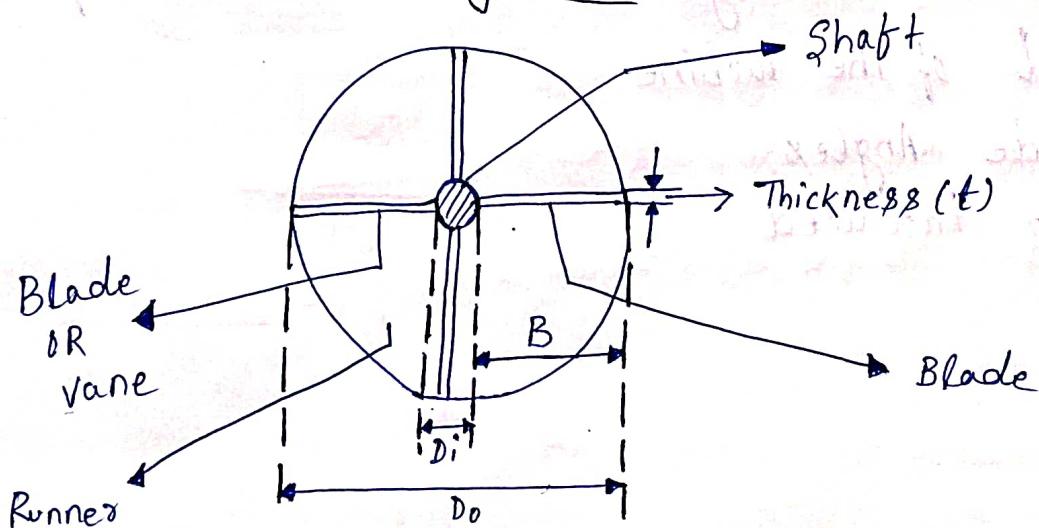
$$= \frac{m (V_{w1} u_1)}{\beta g Q H}$$

$$= \frac{\beta Q (V_{w1} u_1)}{\beta g Q H} = \frac{V_{w1} u_1}{g H}$$

$$\eta_m = \frac{S \cdot P}{R \cdot P} = \frac{P_s}{P_R} = \frac{P_s \times g H}{V_{w1} u_1}$$

$$\eta_o = \eta_m \times \eta_h = \frac{S \cdot P}{W \cdot P} = \frac{P_s}{P_W}$$

Discharge (Q)



$$\text{Total Area} = (A) = \frac{\pi}{4} (D_o^2 - D_i^2)$$

$$D_m = \text{Mean Diameter} = \frac{\pi}{4} (D_o + D_i)(D_o - D_i)$$

$$B = \text{Width Diameter} = \pi \left[\frac{D_o + D_i}{2} \right] \left[\frac{D_o - D_i}{2} \right]$$

$$= \pi D_m B$$

$$(\text{Discharge}) Q = \pi D B V_f$$

$$Q = A V$$

$$D_1 \pi B_1 V_{f1} = D_2 B_2 V_{f2} \pi$$

$$\Rightarrow Q = D_1 B_1 V_{f1} = D_2 B_2 V_{f2}$$

$$Q = \pi (D - z t) B V_f$$

Z = No. of Blade

t = Thickness

D = Mean Dia

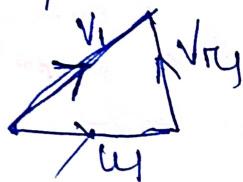
VELOCITY TRIANGLE

→ Francis Turbine -

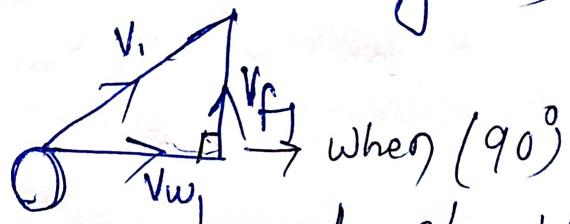
Always Remember

→ Absolute velocity (V) is the resultant of bucket speed (w) and Relative Velocity (v_r)

Ex:-



or



→ Absolute velocity (V) is a resultant of flow velocity and bucket speed!